



Overview over the different measurement methods for geometry error correction for measuring machines and machine tools

Eugen Trapet, ISM3D, Spain eugen@trapet.de, www.trapet.de



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ISM3D: Measurement service and training provider in the north of Spain (I++) and compensated (with own artefacts)







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- **Trapet Precision:**
 - Metrology engineering, artifact development and manufacturing, correction software tools (compensation module for integration), uncertainty evaluation tools (Virtual CMM for integration)



Contents

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- Errors to deal with linear axes -

 - rotary axes
 rigid body model errors
 non-rigid-body model errors
- Applying corrections ("standard formats")
- Measurement devices and methods direct selective methods X Y X (displacement or position) angle (displacement or position) -
 - indirect analytic methods X Y Z (displacement or position)
- Verifying corrections and maintaining corrections valid -
- Conclusions -













Courtesy: ETALON





All errors before compensation and remeasured with compensation active, courtesy: AFM-Tec









3D ball beams and self-centring probe





3 errors "at once", 6 in combination with several beam positions

10-30 minutes per axis

Uncertainty of probe: < 0.0006 mm



from project "MT-Check"

Courtesy: IBS-PE



Measurement of rotary axes with self-centring probe



Problem: the exact location & squareness of a rotary axis is not well known at the micrometre level of 5 axis machine tool.





Courtesy: IBS-PE

Video!

Swivel head machine (large machines) Trunnion table machine (large and small exist)







Ball plate for full error correction, tactile measurement in typically 8 hours







Ball plate for full error correction, optical measurement in typically 2-3 hours

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Ball plate for full error correction, output of so called *.exc format, directly read by correction module



VALL 100 010







Martine a standard (1996). In an anna anna anna anna anna anna ann	Straightness Measurement				Videos!
ALLEY STREET STOLEN STREET STR	range: Straightness accuracy:		±0.3mm		±0.3mm
And the second s			±(0.5µm + 0.1µm/m) or 1% of max measured error		±(0.5µm + 0.1µm/m) or 1% of max measured error
	Straightness resolution:		0.1µm		0.1µm
	Measurement Distance:		25m		25m
	Squareness Measurement		±(1.0 arcsec + 0.2 arcsec/measured travel in meters)		
	Accuracy:				±(1.0arcsec + 0.2 arcsec/ measured travel in meters)
	Angularity Measurement				
	Measurement range:		±400 arcsec		±400arcsec
	Angular resolution:		0.1 arcsec		0.1 arcsec
	Measurement Distance:		25m		25m
RA P	Pitch and Yaw measurement accuracy:		±(0.5 arcsec + 0.05 arcsec/m) or 1% of max measured error		±(0.5 arcsec + 0.05 arcsec/m) or 1% of max measured error
	Roll measurement accuracy				±0.5 arcsec
	(for Horizontal axes only)				or 1% of max measured error
	Parallelism Measurement				
	Accuracy:		Courtesy: API		±(1.0 arcsec + 0.2 arcsec/measured travel in meters)
	YA		Max Error Before VEC™		Max Error After VEC™
Equivalent to:	×	Machine 1	0.0167 in (0.424 mm)	0.0	0077 in (0.196mm)
	×z	Machine 2	0.0394 in (1.000 mm)	0.0	015 in (0.039 mm)
	<u> </u>	Machine 3	0.0064 in (0.162 mm)	0.0	016 in (0.041 mm)
	xty xxx	Machine 4	0.0208 in (0.527 mm)	0.0	035 in (0.088 mm)
	trans w	Machine 5	0.0121 in (0.306 mm)	0.0	036 in (0.091 mm)
erors of the movement in each point of its traject	h rotatorical		((,



Renishaw's new 6 degree of freedom measuring device.



RENISHAW's brand new 6-degrees-of-freedom error measuring system working title: "6-dof" It is so far UCC2-dependent. This is an advantage as far as automatization is concerned, there is no need for precise alignment (machine follows laser); head size is aprox. 60mm x 60mm x 60mm



















Measuring the errors of the rotary heads of CMMs and og 5 axis machine tools







Courtesy: FIDIA





Verifying a correction and maintaining a correction valid



Not all error measurement methods are suited to verify the same errors measured for the exactness of their correction:

Laser displacement interferometers, straightness measuring systems, and direct distance measuring systems as well as artefacts are well suited

Machine design may substantially favour the accuracy of correction measurements, the stability of errors over time and facilitate the use of the corrected machine

Most important a design taking temperature and temperature changes into consideration; Low CTE scales are the most important improvement ...of course together with work piece temperature compensation.

"compensating work piece temperature at the level of uncertainty of 1 °C is easier than compensating during the calibration of the machine at the level of uncertainty of 0.3 °C or even when calibrating a steel standard at the level of uncertainty of < 0.1 °C !"

Reference structures in/on the machine and external reference objects measured e.g. by the machine allow to judge the stability and facilitate low order tuning values (for example for squareness changes and gradient induced pitch)



Verifying a correction and maintaining a correction valid



Use of simple artifacts, measured with the machine,

ISMED

here: balltetrahedron



For CMMs the "full" correction exists since about 30 years and is indispensable today for the accuracy;

On site calibration become more feasible with the new calibration methods and thus a higher accuracy for a larger number of CMMs;

This goes hand in hand with more thermally stable designs of the CMMs and with the capability of the user to monitor his machine accuracy (artefacts)

The "full scale" correction of machine tools has just started and has great potential still, many controllers have full error correction now, for high accuracy part machining it is already indispensable.

In order to monitor the machine tool accuracy the users will more and more rely on periodic verifications (e.g. by artefact measurement)

Correction parameter measurement has evolved from a tedious job of 1 week to a profitable 1 day's job (profitable for service and client)